RANS, URANS and LES calculations through five by five mixing grids of nuclear fuel assembly

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Outlook

□ Fuel assemblies issues

□ First LES through a 2x2 mixing grid – need for validation

□ LES/URANS through 5x5 mixing grid – KAERI grid

□ RANS simulations through a 5x5 mixing grid

Conclusions and perspectives

Fuel assemblies issues



Fuel assemblies issues

□ Reliability and performance of Fuel assemblies in the core

25 days of non-availability due to problems concerning the fuel assemblies (2008)

2 major problems



Fretting (vibrations)



Fuel assemblies issues

□Complex geometry

Different Fuel Assembly models

Several producers

□Many constraints

Low head loss

Good heat exchange

Low vibration

Use Computational Fluid Dynamics (CFD) to obtain detailed flow structures

Validate by comparing CFD results with experiment when available/possible on some known configurations











$$\left(m_{add} + \frac{\lambda L}{2}\right)\frac{d^2 a_n}{dt^2} + \frac{n^4 \pi^4 EI}{2L^3}a_n = F_n(t)$$





- LES seems reliable, the qualitative results are satisfactory (displacement of few microns)
- Need for validation



DSP : comparison to experimental results (1st span)



Observation : RANS models underestimate the turbulent kinetic energy on this case





- □ KAERI experiment MATHIS-H (horizontal)
- Benchmark organized by OECD
- □ Split-type vane, 5x5 mixing grid, scale 2.67
- Few doubts about the symmetry of the configuration (the grid is too close to the outlet)



 \Box Reynolds number Re_H=50000 62 Million cells











F

z = 0.5D_H

 $z = 4D_{H}$



LES with a pure centered scheme is the only one showing a split-like vane behavior with the turbulent kinetic energy



□ This is a part of a benchmark organized by EPRI (Manivel experiment conducted at EDF)





Fully hex mesh



Main characteristics :





□ 2 types of junctions between the two different grids :

conforming junction with mixed elements (hex, tets and pyramids
Non-conforming junction





Turbulent kinetic energy evolution

Code Saturne User Club - 09/04/2013



- □ Results with 2nd moment closure and a standard wall function with 1 velocity scale
- Global underestimation of the headloss coefficient except for the bare bundle
- □ Same results with the two types of junction



		RSM 1	k-ε 2	k-ε 1	RSM 2	kω-
	Exp	scale	scales	scale	scales	SST
DPM1	1,628	1,361	1,107	1,412	1,011	1,115
DPM2	0,570	0,573	0,417	0,584	0,387	0,444
DPM3	1,606	1,391	1,089	1,440	0,993	1,126
DPM4	0,813	0,678	0,562	0,708	0,521	0,554
DPM5	1,621	1,391	1,089	1,440	0,993	1,126
DPM6	0,782	0,678	0,562	0,708	0,521	0,554

- □ Sensitivity to the turbulence model and wall functions
 - □ 1 scale results are closer to the experimental data
 - □ Is this phenomena due to the junctions?

With only simple grids (conforming mesh), the results concerning the under-estimation of the head-loss coefficient are worse! And there is still an underestimation with the wall function using 2 scales ...



Conclusions and perspectives

- RANS does not seem adequate to predict the flow through mixing grids (neither for head-loss coefficient nor for turbulent kinetic energy level)
- URANS might be used (good qualitative behavior) but given an overestimation of the turbulent kinetic energy what is not suitable if one expects to study vibrations or heat transfer
- LES with a pure centered scheme and a dynamic Smagorinsky model gave the best quantitative results for the KAERI grid used during the OECD benchmark
- □ LES gave good qualitative behavior for vibration predictions
- More validation is still needed in particular concerning the pressure along the rods